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深部煤层 CO₂ 注入煤岩力学响应特征及机理研究进展

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摘要: 为揭示 CO₂ 注入煤岩力学响应特征及机理, 回顾了 CO₂ 注入煤岩力学性质影响因素、CO₂ 注入对煤岩大分子-孔隙-裂隙结构改造作用和煤岩力学参数的统计模型、理论模型与智能预测模型。结果表明: CO₂ 注入煤岩力学性质受控于煤阶、CO₂ 压力、水分、围压和时间等因素, CO₂ 注入压力的增高、水的加入及时间的延长均会进一步降低煤岩力学性质, 而围压对 CO₂ 注入力学性能弱化具有一定改善作用。CO₂ 水溶液通过溶胀作用、萃取作用和塑化作用促使煤岩大分子结构重组, 通过微晶结构改变、化学溶蚀和非均匀变形改造煤岩孔隙结构, 通过化学溶蚀、膨胀应力和化学-应力耦合作用诱发煤岩结构损伤, 均不同程度引起煤岩力学性能弱化。在 CO₂ 注入煤岩力学参数预测模型中, 类 Langmuir 模型、广延指数模型和修正的粘聚力模型具有明确的物理意义, 而智能预测模型具有更高的预测精度, 预测准确度可达 99% 以上。本次研究为科学评价 CO₂-ECBM 安全性和促进深部煤层 CO₂ 高效注入奠定了理论基础。

关键词: CO₂-ECBM; 力学性质; 弱化机理; 多尺度结构; 预测模型; 油气地质。

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Mechanical Response Characteristics and Mechanism of Coal-Rock with CO₂ Injection in Deep Coal Seam: A Review

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Abstract: To reveal the mechanical response characteristics and mechanisms of coal-rock with CO₂ injection, the influencing factors of mechanical properties of coal-rock with CO₂ injection, the transformation effect of CO₂ on the macro molecular-pore-fracture structure of coal-rock and the statistical model, theoretical model and intelligence prediction model of mechanical

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parameters of coal-rock with CO₂ injection were reviewed. Results show that mechanical properties of coal-rock with CO₂ injection are controlled by the coal rank, the CO₂ pressure, the moisture, the confining pressure and the time. The increase of CO₂ injection pressure, the addition of water and the extension of time can further reduce the mechanical properties of coal-rock with CO₂ injection, while the confining pressure can ameliorate the weakening effect of mechanical property to a certain extent. The CO₂ aqueous solution recombines the macro molecular structure of coal-rock by the swelling, extraction and plasticization effects, reforms the pore structure of coal-rock by the micro crystalline structure change, chemical corrosion and non-uniform deformation effects, damages the fracture structure by the chemical corrosion, swelling stress and chemical-stress coupling effects, which all weaken the mechanical properties of coal-rock in varying degrees. Among the prediction models of mechanical parameters of coal-rock with CO₂ injection, the Langmuir-like model, the extended exponential model and the modified cohesion model have clear physical significance, while the intelligence prediction model has higher prediction accuracy, and the prediction accuracy can reach more than 99%. This study lays a theoretical foundation for scientifically evaluating the CO₂-ECBM safety and promoting the efficient injection of CO₂ into deep coal seams.

Key words: CO₂-ECBM; mechanical property; weakening mechanism; multi-scale structure; prediction model; petroleum geology.

0 引言

我国埋深 2 000 m 以浅的煤层气资源总量为 36.8×10^{12} m³, 其中埋深在 1 000~2 000 m 的深部煤层气资源量占 51.2% (李松等, 2016). 煤层 CO₂ 地质存储与 CH₄ 强化开采 (CO₂-ECBM) 技术通过 CO₂ 的吸附-置换-驱替作用可显著提高深部煤层气的抽采率, 同时, 作为碳捕集、利用与封存 (CCUS) 中的重要一环, 该技术又可实现碳封存 (Niu, 2019; 任京伟等, 2020; 桑树勋等, 2020; Niu *et al.*, 2019, 2021, 2022), 集新能源开发和环境保护于一体 (Zhu *et al.*, 2021). 我国已在沁水盆地和鄂尔多斯盆地东缘等进行了 CO₂-ECBM 示范工程探索 (Pan *et al.*, 2018), CO₂-ECBM 技术的系统开展将助力我国碳减排, 有望在碳达峰和碳中和目标实现中扮演重要角色.

自 Fulton *et al.* (1980) 提出注 CO₂ 提高煤层气抽采率的理念之后, 国内外学者主要围绕 CO₂-ECBM 的有效性、经济性、长期性和安全性展开大量研究. 特别是近 20 年来, 研究聚焦于 CO₂/CH₄ 气体吸附解吸-扩散渗流-置换驱替过程、煤基质膨胀应力应变效应、煤储层微观结构及力学性质响应等方面 (朱立, 2014; 牛庆合等, 2018; 桑树勋, 2018; Niu *et al.*, 2019; 张臣等, 2019), 为 CO₂-ECBM 机理认识、技术优化及 CO₂ 可注性和封存容量评估奠定了基础.

CO₂-ECBM 安全性是其规模化实施的根本保障. 深部煤储层具有高地温、高储层压力和高地应力的“三高”特点, 所注入的 CO₂ 常以超临界状态存

在 (温度 > 31.1 °C, 压力 > 7.38 MPa). 超临界 CO₂ 和储层水形成的溶液更易与煤储层发生复杂物理化学反应, 引起煤层力学性能弱化 (吴迪等, 2015; 杜玉昆等, 2019; 何立国和杨栋, 2021). 加上煤层吸附膨胀应力应变效应, CO₂ 注入直接改变煤储层原始应力状态, 产生附加位移, 引起煤储层变形破裂 (Niu *et al.*, 2017), 诱发一系列次生灾害, 如 CO₂ 泄漏 (赵健等, 2021)、断层活化 (周军平等, 2019) 和场地变形失稳 (白冰, 2008) 等 (图 1). 另外, CO₂ 封存是一个长期的过程, 这决定了 CO₂-ECBM 所面临安全性问题必将随着时间的推移而持续显现.

然而, 目前针对 CO₂ 注入煤岩力学响应规律及弱化机理不明, 以致缺乏深部煤层 CO₂-ECBM 安全性的有效评估理论依据, 成为制约 CO₂-ECBM 技术规模化、产业化的关键之一. 于此, 本文通过评述 CO₂ 注入煤岩力学性质影响因素、煤岩大分子-孔隙-裂隙多尺度结构响应特征和 CO₂ 注入煤岩力学参数预测模型等研究进展, 以期进一步深化 CO₂-ECBM 安全性的基础理论研究.

1 煤岩力学性质影响因素

CO₂ 注入煤层力学性能发生弱化, 已得到国内外学者们的证实. 前人研究主要关注煤岩的宏观力学参数, 重点研究峰值强度、弹性模量和泊松比的变化, 认为 CO₂ 注入后煤岩峰值强度和弹性模量降低, 泊松比升高 (表 1). 尽管 CO₂ 注入引起的煤岩力学性能弱化效应已达成共识, 但文献中力学参数变化值从百分之几到百分之几十不等, 具有较大离散性, 这与 CO₂ 注入煤岩力学参数影响因素众多密切相关 (如煤阶、CO₂ 注入压力、水分、围压和时间等).

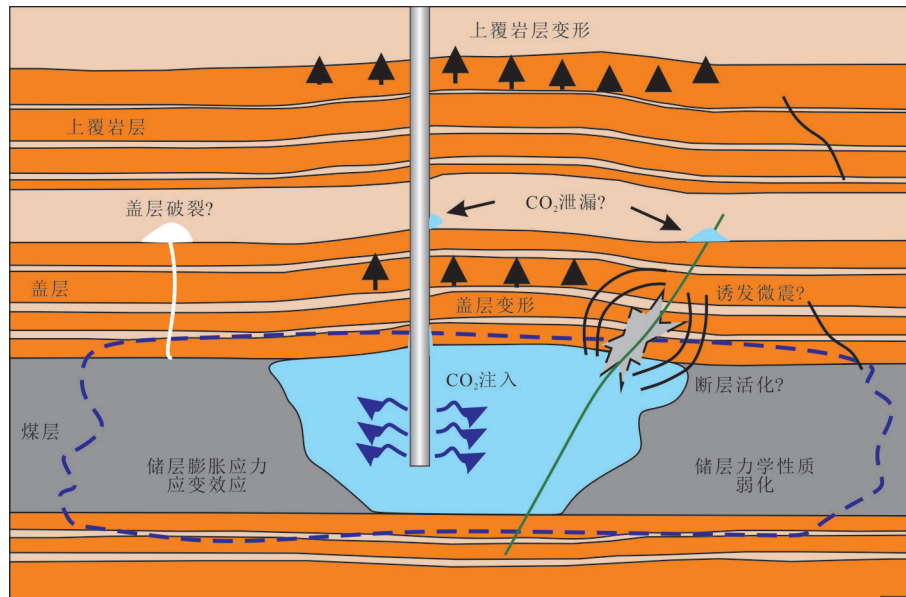


图 1 CO₂注入煤层地质力学响应及潜在安全性问题

Fig. 1 Geomechanical response and potential security issues of coal seam with CO₂ injection

表 1 CO₂注入煤岩力学性质影响因素及规律

Table 1 Influencing factors and laws of mechanical properties of coal-rock with CO₂ injection

影响因素	实验条件	煤岩分类	范围	$\Delta S(\%)$	$\Delta E(\%)$	$\Delta \mu(\%)$	Δc (%)	$\Delta \varphi$ (%)	数据来源
CO ₂ 注入压力	单轴、室温	褐煤	1~3 MPa	3~10↘	3~16↘	-	-	-	Perera <i>et al.</i> , 2011
	单轴、33 °C	烟煤	3~16 MPa	44~78↘	20~72↘	-	-	-	Perera <i>et al.</i> , 2013
	三轴、室温	褐煤	5 MPa	15↘	41↘	-	20↘	5↘	陈德飞, 2014
	三轴、22 °C	-	0.2~5.5 MPa	2~46↘	6~32↘	-	-	-	Masoudian <i>et al.</i> , 2014
	单轴、35 °C	褐煤	2~10 MPa	6~61↘	16~44↘	10~62↗	-	-	Ranathunga <i>et al.</i> , 2016a
	三轴、40 °C	无烟煤	8 MPa	54↘	41↘	65↗	-	-	贾金龙, 2016
	单轴、40 °C	无烟煤	2~8 MPa	34~80↘	29~83↘	-	-	-	Zagorščak and Thomas, 2018
	三轴、50 °C	烟煤	12 MPa	17↘	21↘	-	16↘	2↘	Meng and Qiu, 2018
	单轴、37 °C	烟煤	2~10 MPa	34~63↘	34~66↘	9~31↗	-	-	Zhang <i>et al.</i> , 2019a
	三轴、40 °C	无烟煤	4~8 MPa	47~63↘	32~50↘	-	-	-	牛庆合, 2019
	单轴、25 °C	烟煤	0.2~2 MPa	8~48↘	-	-	-	-	Zhou <i>et al.</i> , 2020
水分	单轴、37 °C	烟煤		59/68↘	62/71↘	26/38↗	-	-	Zhang <i>et al.</i> , 2019a
	三轴、37 °C	烟煤	干燥/饱水+CO ₂	19/23↘	18/20↘	-	-	-	Zhang <i>et al.</i> , 2019b
	三轴、40 °C	无烟煤		47/64↘	32/55↘	19/28↗	-	-	Niu <i>et al.</i> , 2021
围压	三轴、室温	褐煤	0~10 MPa	19~2↘	21~0↘	-	-	-	Viete and Ranjith, 2005
	三轴、35 °C	褐煤	0~10 MPa	31~10↘	28~13↘	-	-	-	Ranathunga <i>et al.</i> , 2016a, 2016b
	三轴、37 °C	烟煤	0~11 MPa	39~17↘	41~17↘	-	-	-	Zhang <i>et al.</i> , 2019a, 2019b
时间	单轴、室温	-	25~45 d	42~65↘	24~43↘	-	-	-	Bagga <i>et al.</i> , 2015
	单轴、50 °C	无烟煤	5~30 d	50~67↘	50~63↘	-	-	-	贺伟, 2018
	单轴、40 °C	褐煤	1~45 d	13~23↘	-	-	-	-	Sampath <i>et al.</i> , 2019a
	单轴、35 °C	烟煤	1~13 d	16~47↘	11~40↘	-	-	-	Su <i>et al.</i> , 2020
	三轴、35 °C	褐煤	21~288 d	44~50↘	59~69↘	-	-	-	Ranathunga <i>et al.</i> , 2016b

注: ΔS 、 ΔE 、 $\Delta \mu$ 、 Δc 和 $\Delta \varphi$ 分别代表峰值强度、弹性模量、泊松比、粘聚力和内摩擦角等力学参数的变化百分比, 计算公式为 $\Delta f = |f_1 - f_0| / f_0 \times 100\%$, f 代表力学参数, 下标 1 和 0 代表流体注入后和流体注入前; “↘”、“↗” 分别代表力学参数降低和升高; “/” 前、后的数据分别代表干燥、饱水+CO₂状态下力学参数。

1.1 煤阶

煤阶是表征煤变质程度的重要参数,煤阶越高煤变质程度越大.煤的显微组分和孔裂隙结构随变质程度发生改变,一般认为,随镜质组反射率的增大,煤的水分、挥发分逐渐减少而碳含量增大(Li *et al.*, 2017),中孔、大孔逐渐减少而微孔逐渐增多(Moore, 2012),微裂隙不断发育但其非均质性增强(Chen *et al.*, 2015; Wang *et al.*, 2019b).煤不同尺度结构变化直接影响到其初始力学性质和吸附能力,如,在大分子尺度上,煤的变质过程中芳香稠环体系缩合程度增加、侧链/官能团减少,造成结构单元增大且致密,进而提高煤岩单轴抗压强度和弹性模量(Pan *et al.*, 2013);在孔隙尺度上,随着煤阶增大煤中微孔逐渐增多,为气体提供更多吸附场所,促使高阶煤吸附能力增强(Yan *et al.*, 2020a).

通过梳理文献中CO₂注入褐煤、烟煤和无烟煤峰值强度和弹性模量的数据(图2),发现CO₂注入后褐煤的 ΔS 和 ΔE 值最小,其次是烟煤,烟煤的 ΔS 和 ΔE 分别是褐煤的2.17倍和2.83倍,无烟煤的 ΔS 和 ΔE 最大,分别是褐煤的2.08倍和2.32倍,说明煤阶的提高增强了煤岩力学性能弱化效应,这和Ranathunga *et al.*(2016b)研究结论相一致.

注入CO₂煤岩会发生吸附体积膨胀,煤岩吸附膨胀变形可能是其力学强度的衰减原因(Perera *et al.*, 2013),然而进一步的研究表明,煤吸附膨胀应变随着煤阶呈现倒U型关系(Perera, 2017),这与CO₂注入煤岩力学参数随煤阶的演化趋势相悖,说明仅考虑体积膨胀并不能完全解释CO₂注入煤岩力学性能弱化效应.而煤岩的吸附能力和力学参数随

煤阶呈现相似演化规律,证明两者之间具有相关性(Zhou *et al.*, 2020),但要揭示煤岩力学性质弱化机理,需要深入研究CO₂注入煤岩成分和结构的变化规律.割理大量发育促使更多CO₂吸附于基质中(Ranjith and Perera, 2012),减小煤表面自由能,降低裂隙尖端破裂的拉应力阈值,导致高阶煤CO₂注入后更易沿割理方向破裂(Chen *et al.*, 2015).另外,煤中有机组分和矿物的细观力学性质存在较大的差异,如,石英和菱铁矿的压痕模量最大,惰质组、镜质组和壳质组次之,而高岭土的压痕模量最小(Yu *et al.*, 2018; Hou *et al.*, 2020).不同煤阶煤中有机质组分和矿物组分含量及分布变化较大,造成细观力学性质强烈的非均质性,这也不同程度影响了CO₂注入煤岩宏观力学性质.总之,煤的吸附能力、割理发育程度和细观力学性质的非均质特征协同控制CO₂注入煤岩的力学性质.

1.2 CO₂注入压力

CO₂注入压力对煤岩力学性质影响方面已取得显著进展,大量实验结果表明CO₂注入压力对煤岩力学参数具有明显的控制作用(图3),表现在煤岩峰值强度(S)、弹性模量(E)和泊松比(μ)随CO₂注入压力的规律性变化.一般地, ΔS 和 ΔE 随着CO₂注入压力先快速增大、后缓慢增大直至趋于平稳(Masoudian *et al.*, 2014; Ranathunga *et al.*, 2016b; 牛庆合, 2019; Zhou *et al.*, 2020).温度高于沸点低于临界温度、压力低于临界压力条件下的CO₂处于亚临界状态,亚临界CO₂和超临界CO₂流体性质存在较大差异.考虑深部煤层CO₂的超临界状态,学者们着重探讨注亚临界CO₂和超临界CO₂对煤岩力学性

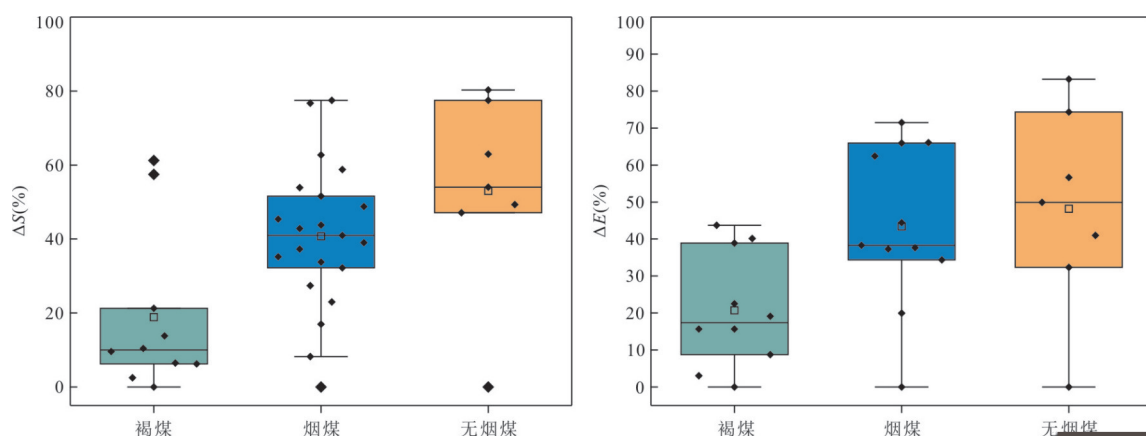


图2 不同煤阶煤CO₂注入后峰值强度和弹性模量变化规律

Fig. 2 Variations of peak strength and elastic modulus of different rank coals with CO₂ injection

数据来源:褐煤,Perera *et al.*, 2011;陈德飞,2014;Ranathunga *et al.*, 2016a;烟煤,Perera *et al.*, 2013;Zhang *et al.*, 2019a;Zhou *et al.*, 2020;无烟煤,贾金龙,2016;Zagoršcak and Thomas, 2018;牛庆合, 2019

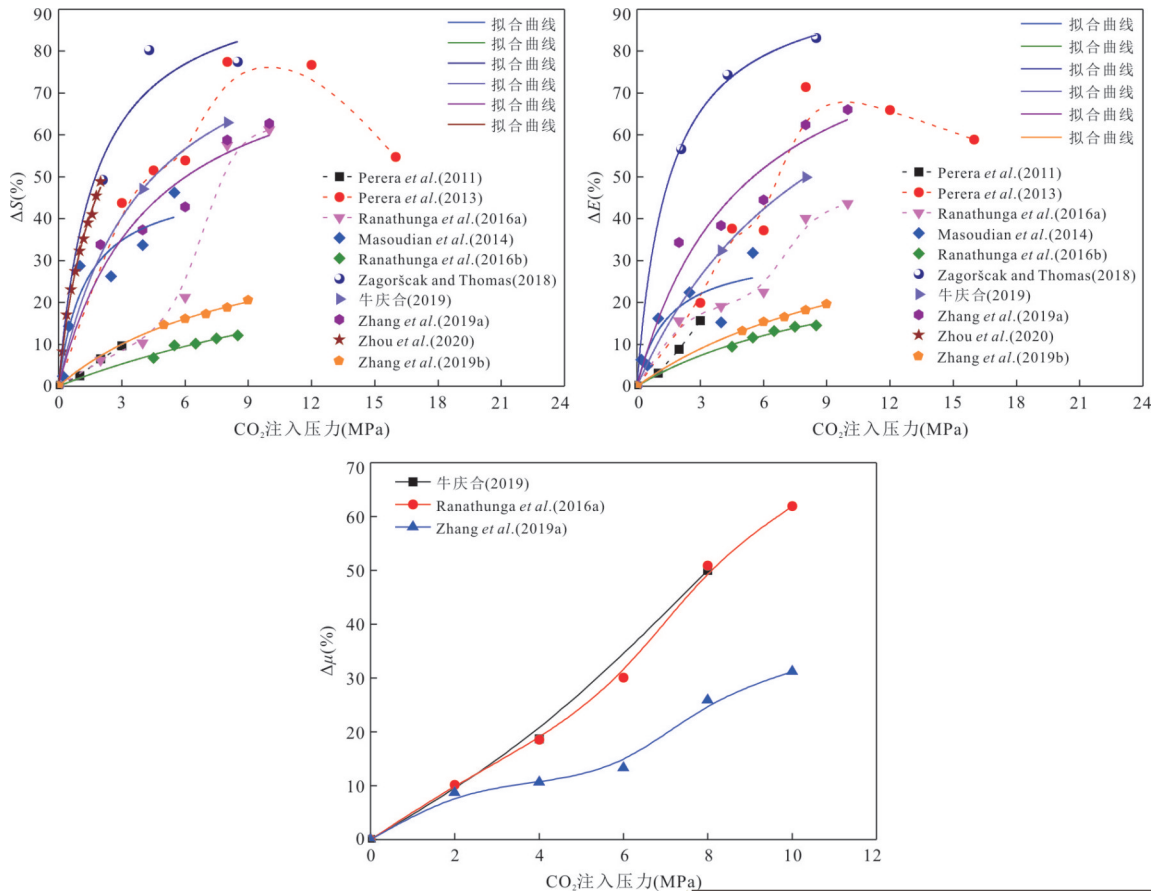


图 3 CO₂注入压力对煤岩力学参数的影响

Fig. 3 Influence of CO₂ injection pressure on mechanical parameters of coal-rock

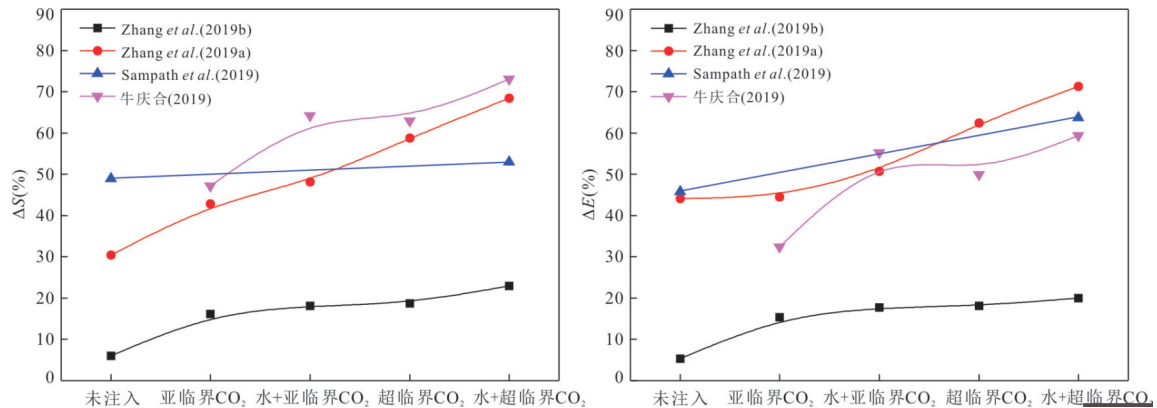
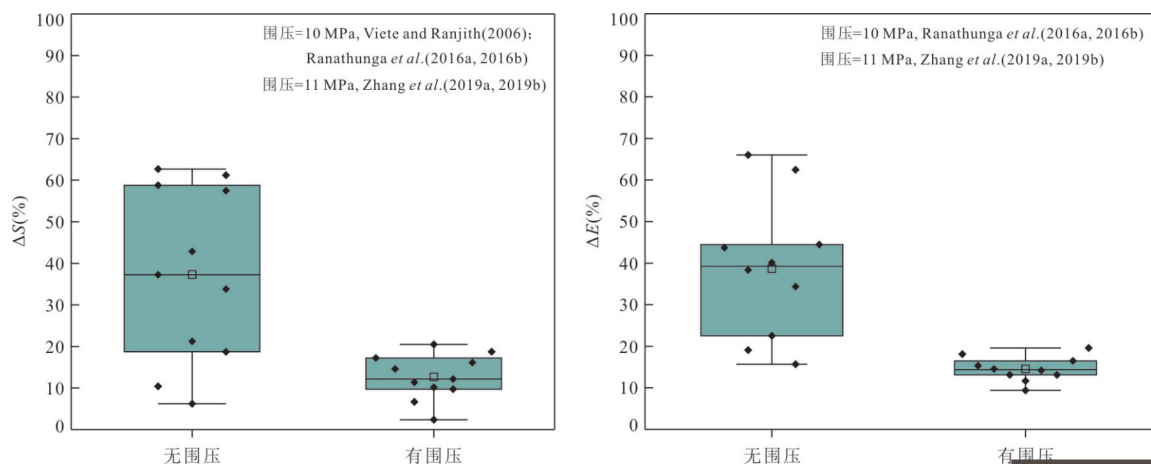
质的影响,但目前研究存在一定争议.如,同等条件下,部分学者研究表明超临界 CO₂注入煤岩峰值强度要比注亚临界 CO₂降低 40%~46% (Perera *et al.*, 2013; Ranathunga *et al.*, 2016a),证实超临界 CO₂对煤岩力学性能的弱化效应更强,而另外学者认为 CO₂注入压力达到 4.3 MPa 时煤岩的 ΔS 和 ΔE 即接近最大值,在超临界阶段煤岩力学性质趋于稳定 (Zagorščak and Thomas, 2018),但由于数据有限,该观点仍需进一步验证.

实际上,CO₂注入对煤岩力学性质的影响具有阶段性 (Perera *et al.*, 2013),煤岩峰值强度和弹性模量在亚临界 CO₂阶段快速衰减直至趋于稳定,在亚临界和超临界过渡阶段再次迅速降低,在超临界阶段有所恢复.超临界 CO₂强烈的塑化能力促使煤岩力学性能显著弱化,而继续注入高压 CO₂提升孔隙压力、对煤基质产生一定程度的压缩 (Pan and Connell, 2007),抑制了 CO₂吸附对煤岩内部结构的改造,致使高压 CO₂阶段煤岩峰值强度和弹性模量有所回升.关于 CO₂注入煤岩泊松比的研究较

少,目前已获得的数据显示 Δμ 和 CO₂注入压力之间几乎呈现线性正相关关系,表明提升 CO₂注入压力将持续增强煤岩受载时横向变形能力.

1.3 水分

针对深部含水煤层,探索水对 CO₂注入煤岩力学性质的影响也是研究焦点之一.前期研究重点探讨注水、亚临界 CO₂、超临界 CO₂及其混合流体对煤岩峰值强度和弹性模量等力学参数的影响 (图 4).事实上,煤岩仅注水也会发生力学性能弱化,如,在饱水后煤岩峰值强度可降低 5.99%~48.89%,而弹性模量可降低 5.36%~45.80% (Sampath *et al.*, 2019a; Zhang *et al.*, 2019a, 2019b).煤在吸附水分子之后同样发生膨胀变形 (Fry *et al.*, 2009; Liu *et al.*, 2016),造成煤岩矿物和有机质结构改变,引起力学性能弱化.注水煤岩形成的局部力学薄弱区往往是煤岩内部的起裂位置 (Zhang *et al.*, 2018).然而,水分子主要吸附在煤基质极性吸附位 (含氧官能团等),随煤阶增大,极性吸附位减少,水分的吸附量降低 (韩思杰和桑树勋, 2020),这也是 Zhang *et al.*

图4 水分对CO₂注入煤岩力学参数的影响Fig. 4 Influence of water on mechanical parameters of coal-rock with CO₂ injection图5 围压对CO₂注入煤岩力学参数的影响Fig. 5 Influence of confining pressure on mechanical parameters of coal-rock with CO₂ injection

(2019a, 2019b) 研究所得的注水后煤岩力学参数变化较 Sampath *et al.* (2019a) 研究结果更小的原因之一。

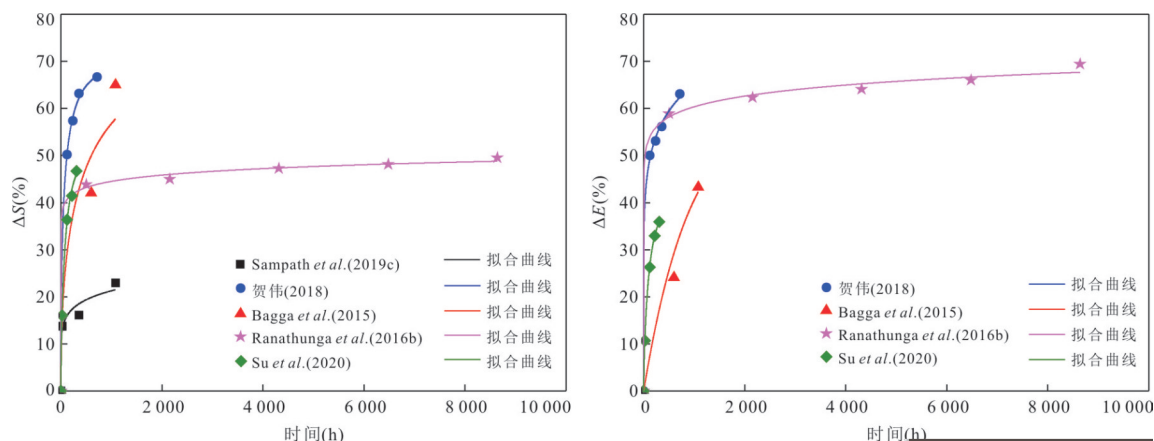
另外, 研究发现CO₂注入于饱水煤样中会引起力学性能更大程度弱化. 水分子和CO₂分子之间虽然存在竞争吸附效应, 但两者均会引起煤岩力学参数降低, 故CO₂和水注入对煤岩力学性能弱化作用更强. 同时, CO₂可溶于水, 特别是超临界CO₂在水中溶解度更大, 可形成pH值更低的酸溶液, 并溶蚀煤中可溶矿物, 形成微观结构缺陷 (Shi *et al.*, 2020), 再加上超临界CO₂具有较强萃取能力, 通过萃取煤中含氧官能团 (如-C=O和-COOH等) 来改变其官能团结构 (王倩倩, 2016), 从而引发超临界CO₂和水注入煤岩力学参数显著降低. 因此, 水分对CO₂注入煤岩力学性质的弱化也起到了促进作用。

1.4 围压

深部煤层承受较大地应力, 研究CO₂注入煤

岩力学性质响应必然要考虑应力的影响. 目前的研究常通过施加围压来模拟地应力条件, 前人也分析了围压对CO₂注入煤岩力学性质的影响. 通过梳理文献中相关研究数据 (图5), 发现有围压情况下注CO₂煤岩的ΔS和ΔE平均值为12.70%和14.55%, 而无围压情况下分别为37.34%和38.67%, 因此, 有围压情况下注CO₂煤岩的ΔS和ΔE仅是有围压情况下的34.01%和37.62%, 证实施加围压对CO₂注入煤岩力学性能弱化具有明显的抑制作用, 这与Masoudian *et al.* (2014) 和Wang *et al.* (2013) 的研究结论一致。

围压对CO₂注入煤岩力学性质的影响与煤岩围压硬化效应和吸附能力降低有关. 煤岩的峰值强度随围压增大而逐渐提高 (崔聪等, 2018), 依据Hoek-Brown准则, 高围压作用下煤岩显然更难遭到破坏. 另外, 在围压作用下, 煤岩内部孔裂隙结构被压缩甚至闭合, 降低其渗透能力和CO₂

图6 时间对CO₂注入煤岩力学参数的影响Fig. 6 Influence of time on mechanical parameters of coal-rock with CO₂ injection

吸附空间,导致受载煤岩的CO₂吸附能力显著减弱(Wang *et al.*, 2019a),因此,围压对CO₂注入煤岩力学性能的弱化效应具有抑制作用.

1.5 时间

除了地质条件,考虑到CO₂-ECBM的长期性,CO₂注入煤岩力学性能弱化的时效性也引起了关注.时间对CO₂注入煤岩力学参数影响的研究结果见图6,其中,煤岩CO₂注入时间从几天到几百天不等.研究发现较短时间内CO₂注入已对煤岩力学性质产生显著影响,在CO₂注入前3d之内煤岩的峰值强度和弹性模量急剧衰减,可达到最大衰减值的30%~69%左右,这与煤岩的吸附平衡时间基本一致(戚灵灵等, 2015),印证了CO₂吸附是煤岩力学性质降低的直接诱发因素.

CO₂注入煤岩力学参数随时间的阶段性变化和CO₂在煤中的扩散-渗流过程有关(Li *et al.*, 2019),短时间内CO₂运移主要通过达西渗流,控制煤岩力学性质变化的主要原因是煤岩内部非均匀膨胀变形及附加膨胀应力,而CO₂长期运移主要通过菲克扩散,改变煤岩力学性质的原因是矿物溶蚀及大分子结构松弛.这一研究对揭示长期CO₂-ECBM过程中煤岩力学性质响应机理具有重要的意义.

2 CO₂注入煤岩力学性能弱化机理

CO₂注入煤岩力学性能弱化和煤岩内部结构改变密切相关,然而,煤是由多种结构形式有机物和不同种类矿物质组成的混合物,具有大分子、孔隙和裂隙的复杂内部结构.前人采用多种手段研究CO₂注入煤岩多尺度结构响应,试图揭示CO₂注入煤岩力学性能弱化机

理,目前也取得了积极的研究进展.

2.1 大分子结构响应层面

煤是一种天然大分子交联聚合物,而CO₂是一种良好的塑性剂,类似于聚合物中加入塑性剂降低聚合物强度(Larsen, 2003),CO₂注入煤中增加其大分子结构的塑性,进而降低其力学强度.学者们采用CT、XRD、Raman、FTIR等手段研究了CO₂注入煤岩微晶结构、芳香结构、官能团结构的演化特征(Kolak *et al.*, 2015; 杜艺等, 2018; Sampath *et al.*, 2020),均认为CO₂和煤基质之间的反应(如溶胀作用、萃取作用和塑化作用)可改变其大分子结构,表现在:增大晶体面网间距(王恬等, 2018),萃取低分子碳氢化合物(姜仁霞等, 2016),降低弱极性官能团含量(Zhang *et al.*, 2017a),促进侧链断裂和大分子结构重组等(Karacan, 2003).这个过程中,煤大分子定向性降低,结构更加疏松,分布更加紊乱,在受载情况下更容易遭到破坏(Guo *et al.*, 2019),故注入CO₂煤岩力学性能减弱.然而,由于CO₂和煤基质之间反应极为复杂,研究结果存在差异,如,一些学者认为CO₂吸附对煤中官能团分布的影响不明显(Mastalerz *et al.*, 2010; 杜锋等, 2015),也有学者发现吸附CO₂煤大分子结构发生改变,且取决于温度、CO₂注入压力和煤阶等多种影响因素(Wang *et al.*, 2017).因此,需要更多的证据来揭示煤岩注入CO₂大分子结构演化对其力学性能弱化的影响机理.

2.2 孔隙结构响应层面

前人采用压汞、液氮吸附和核磁共振等方法分析了CO₂注入煤岩孔隙体积、比表面积、孔径分布、分形维数和连通性的演化规律,认为CO₂注入或其水溶液与煤诱发的微晶结构改变、化学溶蚀和基质

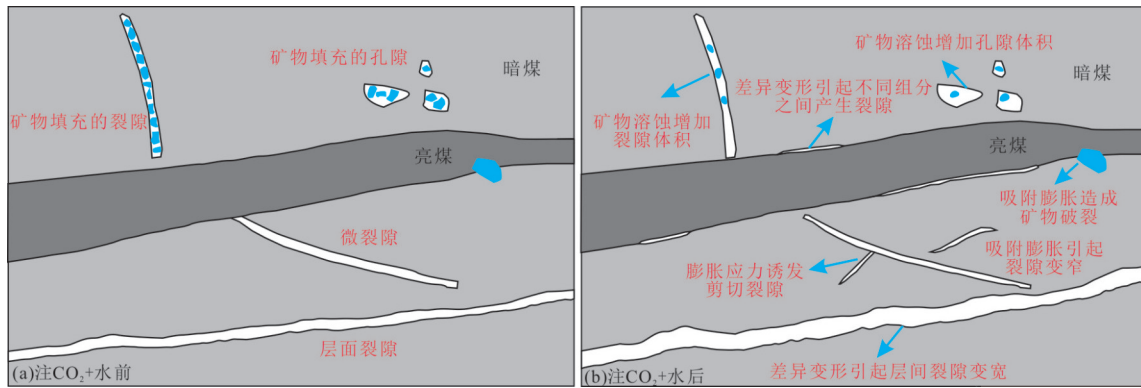


图 7 CO₂注入煤岩内部孔裂隙结构响应模式(修改自 Niu *et al.*, 2021)

Fig. 7 Response pattern of pore-fracture structure in coal-rock with CO₂ injection (modified from Niu *et al.*, 2021)

非均匀变形等作用改造其孔隙结构,且受控于温度、气体压力、水分含量、煤阶和时间等因素的影响。

CO₂-水-煤反应改变了煤岩的微晶结构,主要造成 >0.46 nm 微孔体积增加 (Liu *et al.*, 2019),而 CO₂-水-煤化学溶蚀反应主要引起了 >30 μm 大孔体积的增加,但是化学沉淀也会堵塞孔隙吼道、改变小孔隙的结构 (Zhang *et al.*, 2019c; Du *et al.*, 2020; Zhou *et al.*, 2021). 煤孔隙中填充的矿物在溶蚀和沉淀后,引起基质之间的粘结作用减弱,是造成 CO₂注入煤岩力学性能弱化的原因之一 (Li *et al.*, 2020).

CO₂浸泡后煤岩基质变形造成孔隙体积整体增大(文虎等,2017),表现在微孔向小孔、小孔向中孔、中孔向大孔转化趋势,这与刘长江等(2010)研究一致,但是该变化规律也受煤阶的控制.孔隙孔径的整体增大,提高了煤岩的可压缩性,影响了 CO₂注入煤岩的稳定性.另外,循环向煤中注入 CO₂可使其内部结构发生疲劳损伤并形成新的孔隙,增加孔隙体积 (Su *et al.*, 2021). 孔隙体积的增大提高了煤中 CO₂的吸附量,进一步导致煤岩注入 CO₂力学性质的降低 (Sampath *et al.*, 2019b).

超临界 CO₂和水的共同作用对煤岩孔隙结构的影响最为明显 (杜艺,2018),除了增加大孔体积,还降低孔隙分形维数,减弱其复杂性和非均质性,使孔隙表面更为光滑.该效应弱化了煤微观结构之间的摩擦作用,在高地应力影响下,易形成局部损伤。

2.3 裂隙结构响应层面

CO₂注入煤岩内部裂隙结构发生多重变化,特别是在超临界 CO₂和水共同作用下这种现象更为明显.目前研究认为造成 CO₂注入煤岩裂隙结构演化模式主要有:基质膨胀造成裂隙变窄/闭合、化学溶

蚀引起裂隙扩宽、差异膨胀产生新裂隙、化学-应力耦合造成结构损伤等(图7).CO₂注入后,煤岩内部首先发生基质膨胀,致使原生裂隙被压缩,引起裂隙变窄或闭合 (Zhang *et al.*, 2019d).CO₂水溶液可与煤中矿物(碳酸盐岩和铝硅酸盐等)发生化学反应 (杜艺,2018),促使原生裂隙中充填物溶解,导致充填裂隙重新张开 (Massarotto *et al.*, 2010; 陈润和秦勇,2012; Du *et al.*, 2020),提高煤岩裂隙体积,增加了煤岩结构发生破坏的风险 (杜秋浩等,2019).

煤岩吸附 CO₂后表面自由能降低,依据 Gibbs 吸附方程和 Griffith 失效准则,CO₂注入压力和裂隙扩展所需拉张应力之间存在正相关关系 (Ranathunga *et al.*, 2016b). 吸附 CO₂后煤岩降低了原生裂隙扩展所需拉应力阈值,促进裂隙扩展、煤岩结构损伤;另外,对于深部不可开采煤层,在高地应力作用下,煤岩吸附膨胀诱发的膨胀应力也可造成其结构损伤,如 Zhang *et al.* (2017b) 提出了膨胀应力的计算模型,并预测最大膨胀应力可达 20.52 MPa.

CO₂注入煤岩裂隙也存在多种响应模式,受载条件下煤岩吸附产生的膨胀应力可使其内部矿物发生断裂、产生新裂隙,结合纳米压痕和离散元 (DEM) 方法可再现煤岩内部非均匀膨胀应变引起矿物局部拉伸破坏的过程,进一步揭示煤岩吸附 CO₂膨胀应力产生机理及应力作用下矿物损伤模式 (Zhang *et al.*, 2016). 除了矿物发生破裂,煤的镜质组、惰质组、壳质组及矿物质在 CO₂注入后发生差异变形 (Karacan, 2007),导致不同组分之间产生形状复杂的拉张裂隙,其几何形态受控于矿物的空间展布情况 (Sampath *et al.*, 2019b). 另外,地应力的差异性也会引起 CO₂注入煤岩结构损伤,不同应力路径下 CO₂注入煤岩可发生塑化作用,在孔隙压力和外

部应力的影响下产生剪切裂隙、造成内部结构进一步损伤(Pirzada *et al.*, 2018). 可见, CO₂注入煤岩内部结构改变是温度-应力-渗流-化学多物理场耦合的结果, 故认识CO₂注入煤岩从微观损伤到宏观破坏过程需要从多物理场耦合角度考虑.

3 CO₂注入煤岩力学参数预测模型

3.1 峰值强度和弹性模量预测模型

Langmuir公式常用来表征气体压力和吸附量之间的关系, 由于煤岩吸附气体直接引起基质膨胀变形, 故类Langmuir公式也用来表示不同气体压力下吸附膨胀应变, 目前已应用于CO₂-ECBM数值模拟中(Fang *et al.*, 2019; Liu *et al.*, 2020). 煤岩中注入不同压力的CO₂, 可引起其内部基质吸附膨胀变形, 导致煤岩性质不同程度的劣化(Masoudian *et al.*, 2014), 可采用类Langmuir模型来表征CO₂注入压力和煤岩 ΔS 和 ΔE 的关系:

$$\begin{cases} \Delta S = \frac{\Delta S_{\max} \times p}{p_s + p}, \\ \Delta E = \frac{\Delta E_{\max} \times p}{p_s + p}, \end{cases} \quad (1)$$

式中: p 为气体压力, MPa; ΔS 和 ΔE 分别为无限大压力下煤岩峰值强度和弹性模量降低百分比, %; p_s 为拟合参数, MPa. 该模型可较好拟合Ranathunga *et al.* (2016b)、Zagorščak and Thomas (2018)、牛庆合 (2019)、Zhang *et al.* (2019a)和Zhou *et al.* (2020)实验所得的 ΔS 和 ΔE 数据(图3), 但并不能反映出Perera *et al.* (2013)揭示的较高CO₂压力下煤岩 ΔS 和 ΔE 有所恢复的规律, 因此在较低的CO₂注入压力下, 该模型具有更好的适用性.

煤孔隙结构极为复杂, 气体吸附呈现非线性特征, 单扩散模型和双扩散模型在模拟吸附时间和吸附量上具有局限性. 煤吸附气体所发生的物理变化和溶剂作用于玻璃态聚合物表现出来的粘弹性和溶胀行为类似, 可用模拟玻璃态聚合物弛豫动力学的数学模型来表征煤吸附气体的过程(Staib *et al.*, 2015a). 因此, 采用广延指数模型可用以模拟气体扩散、吸附及基质吸附膨胀行为(Staib *et al.*, 2015b; Czerw *et al.*, 2017; Kiani *et al.*, 2018), 并取得了良好的效果(Miao *et al.*, 2020). 由于煤岩力学性质弱化与气体吸附量之间存在显著的相关性(Niu *et al.*, 2021), 参考气体吸附量吸附量随时间的变化关系, 提出采用广

延指数模型来预测 ΔS 和 ΔE 随时间的变化规律:

$$\begin{cases} \Delta S = \Delta S_{\text{eq}} \left\{ 1 - \exp[-(kt)]^A \right\}, \\ \Delta E = \Delta E_{\text{eq}} \left\{ 1 - \exp[-(kt)]^A \right\}, \end{cases} \quad (2)$$

式中: k 和 A 为拟合参数, 无量纲; t 为时间, d; ΔS_{eq} 和 ΔE_{eq} 是达到吸附平衡状态时煤岩峰值强度和弹性模量的降低百分比, %. 将该模型与文献中数据拟合, 发现具有较高相关性(图6), 故广延指数模型可以用来描述CO₂注入煤岩峰值强度和弹性模量随时间的变化规律.

3.2 粘聚力预测模型

在实际地层条件下, 煤岩的强度受控于有效应力和气体吸附, CO₂注入后有效应力减小和CO₂吸附共同引起原位地层条件下煤岩力学性质降低. 依据Mohr-Coulomb本构模型和Gibbs吸附方程(Perera and Sampath, 2019), 假设CO₂注入对煤岩内摩擦角的影响可忽略不计, 可得CO₂注入煤岩粘聚力预测理论模型:

$$\begin{aligned} C_{\text{CO}_2} = C_0 & \sqrt{\frac{E_{\text{CO}_2}}{E_0} \left(1 - \frac{RT}{\gamma_0 S_E V_M} \int_0^{P_{\text{CO}_2}} (1 - \phi) \frac{V_L}{p + P_L} \right) +} \\ & \frac{1}{2} \sqrt{\frac{1 + \sin \varphi}{1 - \sin \varphi}} \\ & \left[(P_b - \alpha P_0) \sqrt{\frac{E_{\text{CO}_2}}{E_0} \left(1 - \frac{RT}{\gamma_0 S_E V_M} \int_0^{P_{\text{CO}_2}} (1 - \phi) \frac{V_L}{p + P_L} \right) -} \right. \\ & \left. (P_b - \alpha P_{\text{CO}_2}) \right], \end{aligned} \quad (3)$$

式中: C_{CO_2} 和 C_0 分别为CO₂注入煤岩和原始煤岩的粘聚力, E_{CO_2} 和 E_0 分别为CO₂注入煤岩和原始煤岩的弹性模量, R 和 T 分别为摩尔气体常数和温度, γ_0 为原始煤岩的表面自由能, S_E 和 V_M 分别为煤的比表面积和气体摩尔体积, P_{CO_2} 为最大CO₂饱和压力, ϕ 为孔隙度, p 为孔隙压力, V_L 和 P_L 分别为兰氏体积和兰氏压力, φ 为内摩擦角, P_b 为围压, α 为Biot系数.

公式(3)表明CO₂注入煤储层后, 自由态CO₂和吸附态CO₂均导致煤岩强度和应力状态改变, 自由态CO₂改变有效应力、吸附态CO₂降低力学强度, 引起摩尔圆包络线移动, 致使粘聚力降低. 因此, 修正的粘聚力模型不仅可预测CO₂-ECBM中煤岩的粘聚力, 也可借助于摩尔圆变化揭示有效应力和CO₂吸附对煤岩变形破坏的影响机制.

3.3 智能预测模型

自岩石力学智能化理念提出以来(冯夏庭, 1994), 人工神经网络、模糊逻辑、遗传算法、粒子群算法、支持向量机等人工智能模型已在岩石质量指标、弹性模量、抗压强度、岩体质量等级、泊松比和抗剪强度等参数预测中得到了较好的应用(Lawal and Kwon, 2020), 这些模型对预测影响因素多、关系复杂和作用机理不明的研究对象具有独特优势。

考虑到 CO₂-水-煤反应的复杂性及 CO₂ 注入煤岩力学性质受控因素众多, 学者们试图采用人工智能的方法来预测 CO₂ 注入煤岩的力学参数。如, Sampath *et al.* (2019c) 采用人工神经网络(ANN)与自适应神经模糊推理系统(ANFIS)预测出不同 CO₂ 注入压力、煤阶和时间条件下煤岩的单轴抗压强度, 并与线性和非线性多元回归分析等传统方法对比, 发现 ANN 和 ANFIS 预测结果精度更高, 相比传统统计方法具有优越性。Yan *et al.* (2020b) 提出了融合 BP 神经网络、遗传算法和自适应 Boosting 算法的混合人工智能模型, 预测了考虑 CO₂ 注入压力、温度、煤阶和时间等因素影响下煤岩的单轴抗压强度, 并获得 CO₂ 注入煤岩力学性质影响因素的重要性程度, 即, 煤阶 > 时间 > CO₂ 注入压力 > 温度。智能预测模型采用数学方法对大量的实验数据进行训练, 实现对 CO₂ 注入煤岩力学性质的精准预测。

总之, 智能预测模型在 CO₂ 注入煤岩力学参数预测方面具有准确度高的优点, 其预测数据准确度可达 99% 以上, 3.1 节提出的统计模型预测准确度仅在 77% 和 90% 以上, 然而, 智能预测模型在揭示 CO₂ 注入煤岩力学响应机理方面存在天然缺陷。反之, 统计模型和 3.2 节理论模型具有明确的物理意义, 可用来分析 CO₂ 注入煤岩变形破坏及力学性质演化机理。因此, 综合统计模型、理论模型和智能模型预测 CO₂ 注入煤岩力学性质更有意义。

4 结论展望

4.1 主要结论

(1) CO₂ 注入煤岩力学性能发生弱化, 表现在峰值强度、弹性模量降低和泊松比升高。CO₂ 注入煤岩力学性质受控于煤阶、CO₂ 注入压力、水分、围压和时间等因素。CO₂ 注入后褐煤的 ΔS 和 ΔE 值最小, 其次是烟煤, 烟煤的 ΔS 和 ΔE 分别是褐煤的 2.17 倍和 2.83 倍, 无烟煤的 ΔS 和 ΔE 最大,

分别是褐煤的 2.08 倍和 2.32 倍, CO₂ 注入压力增大、水的加入及时间延长均会进一步降低 ΔS 和 ΔE , 但围压对 CO₂ 注入煤岩力学性质弱化具有一定改善。煤岩细观力学性质具有极强非均质性, CO₂ 注入对煤岩有机组分和矿物的细观力学性质影响不同, 评价煤岩细观力学性质可为 CO₂ 注入煤岩力学性能弱化效应的认识提供依据。

(2) CO₂ 注入煤岩力学性能弱化与煤岩大分子-孔隙-裂隙多尺度改变密切相关。CO₂ 水溶液通过溶胀作用、萃取作用和塑化作用促使煤岩大分子结构重组, 通过微晶结构改变、化学溶蚀和非均匀变形改造煤岩孔隙结构, 通过化学溶蚀、膨胀应力和化学-应力耦合作用诱发煤岩裂隙结构损伤, 均不同程度引起煤岩力学性能弱化。

(3) 在 CO₂ 注入煤岩力学参数预测模型中, 类 Langmuir 模型、广延指数模型和修正的粘聚力模型具有明确的物理意义, 且有助于揭示原位地层条件下煤层吸附 CO₂ 后力学性质演化规律和变形破坏响应机制。智能预测模型具有更高的预测精度, 预测准确度可达 99% 以上。综合统计模型、理论模型和智能预测模型可使 CO₂ 注入煤岩力学性质的预测更准确、更有理论和应用价值。

4.2 问题和展望

尽管 CO₂ 注入煤岩力学参数响应特征、力学性质弱化机理和预测模型等方面已开展较多研究, 并取得了积极的认识, 但仍存在一些关键科学问题尚待进一步研究, 如考虑原位地层条件的 CO₂ 注入煤岩宏细观力学性质演化规律, CO₂ 注入受载煤岩变形破坏特征, CO₂ 注入煤岩宏细观力学参数综合预测模型。针对上述问题, 未来可采用气-液-固高温高压反应釜、岩石温度-渗流-应力-化学多场耦合系统等实验设备, 在线 CT 扫描技术、核磁共振、纳米压痕、XRD、Raman 和 FTIR 等测试手段以及 DEM 数值仿真等模拟方法开展以下研究:

(1) 全面认识 CO₂ 注入煤岩宏细观力学响应特征。目前, 关于 CO₂ 注入煤岩力学性质的研究主要聚焦于峰值强度、弹性模量、泊松比这 3 个力学参数, 对其余宏细观力学参数的认识不足。未来可开展 CO₂ 注入煤岩粘聚力、内摩擦角、抗拉强度甚至动态力学性质等研究, 可探究 CO₂ 注入对煤岩硬度、压痕模量和断裂韧度等细观力学性质的影响规律, 基于此, 阐明 CO₂ 注入煤岩宏细观力学参数的动态演化规律。

(2) CO₂注入过程中受载煤岩变形破坏规律研究。CO₂注入煤岩力学性能弱化是煤岩变形破坏这一渐进过程的结果,目前关于CO₂注入受载煤岩内部如何变形、如何发生破坏的认识尚不明晰。未来可通过实验模拟方法实时监测CO₂注入受载煤岩内部渐进变形破坏特征,可借助于数值仿真方法重建CO₂注入煤岩数值模型,再现CO₂注入煤岩应力应变动态变化过程,揭示CO₂注入受载煤岩变形破坏机制。

(3) 系统揭示CO₂注入煤岩力学性能弱化机理。目前,前人已分别从大分子、孔隙、裂隙结构尺度分别阐述CO₂注入对煤岩力学性质的影响,至于何种尺度结构是导致煤岩力学性能弱化的直接原因、CO₂注入煤岩多尺度结构改变和力学参数之间存在何种关系等问题亟待解决。因此,未来可通过建立多尺度结构和力学参数之间的量化关系,结合煤岩宏微观变形破坏特征,从多尺度结构响应及变形破坏特征演化的双重角度共同揭示CO₂注入煤岩力学性能弱化机理。

(4) 建立CO₂注入煤岩力学参数综合预测模型。目前,CO₂注入煤岩力学参数预测模型考虑因素不足,预测精度有限,难以为CO₂封存安全性的评估提供科学依据。因此,基于多因素交互的CO₂注入煤岩力学性质实验结果,完善并修正煤阶、CO₂注入压力、水分、围压、时间和温度等多因素影响下CO₂注入煤岩力学参数的统计模型和理论模型,选取并优化基于多因素交互的CO₂注入煤岩力学参数智能预测模型,实现对CO₂注入煤岩力学参数的综合预测。

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